

Bertram, A. ; Sampaio, R. : A Constitutive Theory for Friction

Frictional laws, describing the contact between continuous bodies, are *constitutive equations*. Within a constitutive theory, we can submit frictional laws to the usual principles (*determinism, objektivty, local action, dissipation*), apply *material isomorphisms* and *symmetry transformations*, and categorize them within the usual classes of materials. Our purpose is to identify the general form of a frictional law as a *material system* in the sence of [2] and thus, obtain all the mentioned concepts. In doing this, we are confronted with the following problems:

- There are always *two* distinct bodies involved in friction. The surface points being coupled may vary all the time.
- In order to describe *sticking* and *sliding* and *no-contact*, the velocity field can be discontinuous with respect to time.
- The cases of *rigid* or *elastic* behaviour are irrelevant in friction.
- Coulomb's law must fit into the theory.

I. Geometry of contact

We consider a solid body eventually being in contact with a surface, which may belong to another body. So, let the *body B* be a 3-dimensional differentiable open manifold. The *boundary* of *B* is dB . On the other hand, let the *surface S* be a 2-dimensional differentiable closed manifold without boundary. The 2-dimensional tangential space (without inner product) to dB is $T_X dB$, and $T^*_X dB$ its dual. *E* is the 3-dimensional *Euclidian space* being endowed with its *translational space V*, a 3-dimensional vector space with inner-product " \cdot ". The *time interval T* is assumed to be an open real interval with elements called *instants*.

A *motion* of the body is a regular time-dependent imbedding $\mu : (B \cup dB) \times T \rightarrow E$ being differentiable on *B*, one-sided differentiable on dB , and piecewise differentiable on *T*. The region occupied by the body *B* at some instant *t* is the set $B_t := \mu(B, t) \subset E$ and, analogously, $dB_t := \mu(dB, t) \subset E$. The differential of μ in $X \in dB$ at $t \in T$ is

$F: T_X dB \rightarrow T_x dB_t \subset V$, being invertible. The past and future *velocities* are the vector fields w^- and w^+ , respectively, being defined on dB_t .

A *motion* of S is a regular time-dependent imbedding $\lambda: S \times T \rightarrow E$ being spacially differentiable and piecewise differentiable with respect to time. The spacial region occupied instantaneously by S is $S_t := \lambda(S, t) \subset E$. In order to exclude *penetration*, we will always assume, that $S_t \cap B_t = \emptyset$. If, eventually, the boundary dB_t and the surface S_t coincide, then they are in contact. The *contact area* is $C_t := S_t \cap dB_t$. Of course, this set might be empty at instants of no contact. The pull-back of C_t on dB is the closed set

$C_0(t) := \{X \in dB \mid \mu(X, t) \in C_t\}$. The past and future velocities of S are u^- and u^+ , respectively. The *relative velocities* are defined as $v^- := w^- - u^-$ and $v^+ := w^+ - u^+$. The following cases are possible for all instants and surface points:

- past or future *sticking*: $v^{-,+} = \mathbf{o}$
- past or future *sliding*: $v^{-,+} \neq \mathbf{o}$ and $v^{-,+} \cdot \mathbf{n} = 0$
- *starting contact*: v^- not defined and v^+ defined
- *loosing contact*: v^- defined and v^+ not defined

The following cases are *not* possible:

- past or future *penetration*: $v^{-,+} \cdot \mathbf{n} \neq 0$

II. Constitutive theory

All the following concepts are local in the sence, that the footpoint $X \in dB$ or $x \in dB_t$ is hold fixed. Let us assume that the body consists of a simple solid material without internal constraints in the sense of [2] and [4]. It may be elastic or inelastic, isotropic or anisotropic, homogenous or non-homogeneous. We consider processes of surface stresses of duration $d \in \mathbb{R}$, starting at a fixed initial state at t_i of the form $s: T \supset [t_i, t_i + d] \rightarrow V$. At each instant, one can decompose s into its normal and tangential part $s = \sigma \mathbf{n} + \tau$. Then we pull τ back to the cotangent space $\tau_0 = F^* \tau \in T^*_X dB$. So each s -process may be equivalently be considered as a (σ, τ_0) -process with values in $\mathbb{R} \times T^*_X dB$. The set of all possible processes of this type forms the *process class* Ω_0 , which is assumed to be closed under restriction and continuation (see [2]),

p. 103). Let $t \neq \mathbf{o} \in T_x dB_t$. Then we call the vector-set $\{v \in T_x dB_t \mid v = \alpha t, \alpha > 0 \in \mathbb{R}\}$ the t -ray. The set of all t -rays, as t runs over the unit-ball of $T_x dB_t$, is denoted by R . The pull back of the relative velocity is defined as the tangent vector $v_o = F^{-1}(v) \in T_X dB$, and

$$D_o := \{\emptyset\} \cup F^{-1}(T_x dB_t) \cup F^{-1}(R) = \{\emptyset\} \cup T_X dB \cup R_o.$$

A *constitutive equation for friction* is a mapping $f : \Omega_o \rightarrow D_o$, such that the push-forward of the values $f(\sigma, \tau_o)$ can be interpreted as the set of *all possible future relative velocities* of the point at the end of a certain (σ, τ_o) -process. So, the values of f can be

- 1) the empty set \emptyset , if there is eventually *no contact*;
- 2) the zero vector $\mathbf{o} \in T_X dB$, if there occurs *sticking*;
- 3) a t -ray, in the case of undetermined *sliding* in the direction of $F t$;
- 4) a tangent vector $v_o \neq \mathbf{o} \in T_X dB$ in the case of *sliding* with relative velocity $F v_o$.

The mapping f , being a constitutive function, is submitted to the principles of rational mechanics. The principle of *determinism* and the principle of *local action* are a-priori fulfilled by the definitions. In order to apply the principle of *material objectivity*, we state that the relative velocity, the normal stress and the tangential stress turn out to be objective, whereas its pull-backs and the (σ, τ_o) -processes are invariant. Thus, the *constitutive equation for friction* f automatically obeys the principle of material objectivity, if, and only if it is the same for all observers (*forminvariance*).

The *principle of dissipation* can be satisfied, if for all admissible s -processes

$$s \cdot v = \tau \cdot v = F \tau_o \cdot F^* v_o = \langle \tau_o, F^* F^* v_o \rangle = \langle \tau_o, v_o \rangle \leq 0$$

holds for all $v_o \in f(\sigma, \tau_o)$. Clearly, this is identically satisfied by the values \emptyset and \mathbf{o} , as in the case of no-contact and sticking, there is no dissipation due to friction.

The triple (Ω_o, D_o, f) is a *material system* in the sense of [2]. By this identification, we can apply all the concepts of material theory to friction, such as *states, aging, revertibility, rate-independence, material isomorphy and symmetry, and isotropy*.

III. Example: a material system of the Coulomb-type

The most well-known and widely applied frictional law is due to COULOMB [3], based on a suggestion by AMONTONS [1]. Let $\sigma_a, \mu_s \geq \mu_k \in \mathbb{R}$ be three positive constants. The stress process class contains all processes starting at some \mathbf{s} and being arbitrarily composed out of the three following types of processes:

(1) no contact: $\mathbf{s} = \mathbf{o} = (\sigma = 0, \tau_{\mathbf{o}} = \mathbf{o})$

(2) sticking: such that $|\tau_{\mathbf{o}}| \leq \sigma_a + \mu_s \sigma$

(3) sliding: $|\tau_{\mathbf{o}}| = \mu_k \sigma$

such that segments of type (3) are following those of type (2), only if equality was reached at the end of the stick-segment. The frictional constitutive equation has the following values

- (1) the empty set \emptyset during segments of no contact;
- (2) the zero vector \mathbf{o} during segments of sticking; and
- (3) the $\tau_{\mathbf{o}}$ -ray during sliding.

References

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